

1.

x-momentum: $0 = -\frac{\partial p}{\partial x} + \rho g \cos \theta + \mu \frac{\partial^2 u}{\partial y^2}$
 $= 0$ since $p_{\text{atm}} = \text{const.}$

$\Rightarrow \tau_{xy} = \mu \frac{\partial u}{\partial y} = -\rho g \cos \theta y + C$

$\tau_{xy}(y=h) = -\rho g \cos \theta h + C = -\tau_{\text{air}}$

$\Rightarrow \tau_{xy} = -\tau_{\text{air}} + \rho g \cos \theta (h-y)$

$\Rightarrow \mu u(y) = -\tau_{\text{air}} y + \rho g \cos \theta (hy - \frac{y^2}{2}) + D$

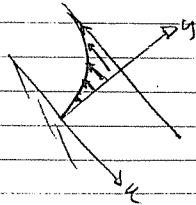
no slip $\Rightarrow u(0) = 0 \Rightarrow D = 0$

$u(y) = -\frac{\tau_{\text{air}}}{\mu} y + \frac{\rho g \cos \theta}{\mu} (hy - \frac{y^2}{2})$

$\tau_{xy}(y=0) = -\tau_{\text{air}} + \rho g \cos \theta h = 0$

$\Rightarrow \tau_{\text{air}} = \rho g \cos \theta h$

$\Rightarrow u(y) = -\frac{\rho g \cos \theta}{\mu} \frac{y^2}{2}$



2. $F(z) = \left(\frac{m-i\Gamma}{2\pi} \right) \ln z$; $z = r e^{i\theta}$

a) $F = \left(\frac{m-i\Gamma}{2\pi} \right) \ln(r e^{i\theta}) = \left(\frac{m-i\Gamma}{2\pi} \right) (\ln r + i\theta) =$

$= \frac{m \ln r + \Gamma \theta + i}{2\pi} - \frac{\Gamma \ln r + m \theta}{2\pi} =$

$= \phi + i\psi$

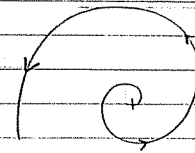
$\Rightarrow$ stream function $\psi = \frac{1}{2\pi} [m\theta - \Gamma \ln r]$

streamlines: $\psi = \text{const.}$

$\Rightarrow m\theta - \Gamma \ln r = m\theta_0 - \Gamma \ln r_0 = \text{const.}$

$\Rightarrow \theta - \theta_0 = \frac{\Gamma}{m} \ln(r/r_0)$

where r_0, θ_0 is a point on the streamline



b) $F(z) = \frac{m-i\Gamma}{2\pi} \frac{1}{z} = \left(\frac{m-i\Gamma}{2\pi} \right) \frac{e^{-i\theta}}{r} =$
 $= \left(\frac{m}{2\pi r} - i \frac{\Gamma}{2\pi r} \right) e^{-i\theta} = (u_r - i u_\theta) e^{-i\theta}$

$\Rightarrow u_r = \frac{dr}{dt} = \frac{m}{2\pi r}$; $u_\theta = r \frac{d\theta}{dt} = \frac{\Gamma}{2\pi r}$



$r \frac{dr}{dt} = \frac{m}{2\pi} \Rightarrow \frac{d}{dt} \left(\frac{r^2}{2} \right) = \frac{m}{2\pi}$

$\Rightarrow \frac{r^2 - r_0^2}{2} = \frac{m}{2\pi} (t - t_0)$

$\Rightarrow r(t) = \sqrt{r_0^2 + \frac{2m}{\pi} (t - t_0)}$

From a) we have $\theta - \theta_0 = \frac{\Gamma}{2m} \ln(r/r_0)^2$

$\Rightarrow \theta(t) = \theta_0 + \frac{\Gamma}{2m} \ln \left(1 + \frac{m}{\pi r_0^2} (t - t_0) \right)$

3.

a) $\frac{\partial u}{\partial t} > 0$; $u \frac{\partial u}{\partial x} = 0$; $v \frac{\partial u}{\partial y} = 0$;

$\omega_z = \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) = -\frac{\partial u}{\partial y} > 0$

$\Gamma = U \cdot L$

b) $x > 0$: $\frac{\partial u}{\partial t} = 0$; $u \frac{\partial u}{\partial x} > 0$; $v \frac{\partial u}{\partial y} = 0$; $\omega_z = 0$

$x < 0$: $\frac{\partial u}{\partial t} = 0$; $u \frac{\partial u}{\partial x} < 0$; $v \frac{\partial u}{\partial y} = 0$; $\omega_z = 0$

$\Gamma = 0$ (since flow is irrotational)

c) $y > 0$: $\frac{\partial u}{\partial t} = 0$; $u \frac{\partial u}{\partial x} = 0$; $v \frac{\partial u}{\partial y} = 0$; $\omega_z > 0$

$x < 0$: $\frac{\partial u}{\partial t} = 0$; $u \frac{\partial u}{\partial x} = 0$; $v \frac{\partial u}{\partial y} = 0$; $\omega_z < 0$

$\Gamma = U_{\text{max}} \cdot L$

4

2D flow $\vec{\omega} = \omega_z(x, y) \vec{e}_z$ $\vec{u} = u(x, y) \vec{e}_x + v(x, y) \vec{e}_y$

$$\vec{\omega} \cdot \nabla \vec{u} = \omega_z \frac{\partial u}{\partial z} + \omega_z \frac{\partial v}{\partial z} = 0$$

$\frac{\partial}{\partial z} = 0$ $\frac{\partial}{\partial z} = 0$

$$\omega_z = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} = \frac{\partial}{\partial x} 0 - \frac{\partial u}{\partial y} = \omega_z(y)$$

$$\frac{D \vec{\omega}}{Dt} = \vec{e}_z \frac{D \omega_z}{Dt} = \vec{e}_z \left(\frac{\partial \omega_z}{\partial t} + u \frac{\partial \omega_z}{\partial x} + v \frac{\partial \omega_z}{\partial y} \right) = 0$$

$\frac{\partial}{\partial t} = 0$ $\frac{\partial}{\partial x} = 0$ $\frac{\partial}{\partial y} = 0$

steady state

$$\nabla \varphi = -\rho_0 \alpha_0 \nabla T = -\rho_0 \alpha_0 \Delta T_0 \nabla \left(\frac{y}{h} \right) = -\rho_0 \alpha_0 \frac{\Delta T_0}{h} \vec{e}_y$$

$$\nabla p = -\rho_0 g \nabla x = -\rho_0 g \vec{e}_x$$

$$\frac{1}{\rho_0} \nabla \varphi \times \nabla p = \frac{\alpha_0 \Delta T_0 g}{h} \vec{e}_y \times \vec{e}_x = -\frac{\alpha_0 \Delta T_0 g}{h} \vec{e}_z$$

$$\frac{\mu_0}{\rho_0} \nabla^2 \vec{\omega} = \frac{\mu_0}{\rho_0} \nabla^2 \omega_z(y) \vec{e}_z = \frac{\mu_0}{\rho_0} \frac{\partial^2}{\partial y^2} \omega_z(y) \vec{e}_z$$

Equation $\Rightarrow 0 = -\frac{\alpha_0 \Delta T_0 g}{h} + \frac{\mu_0}{\rho_0} \frac{d^2 \omega_z}{dy^2}$

$$\omega_z = -\frac{\partial u}{\partial y} = -\frac{U_0}{6h} \left(1 - 3 \left(\frac{y}{h} \right)^2 \right)$$

$$\Rightarrow \frac{d^2 \omega_z}{dy^2} = \frac{U_0}{6h} \cdot \frac{6}{h^2} = \frac{U_0}{h^3}$$

$$\Rightarrow 0 = -\frac{\alpha_0 \Delta T_0 g}{h} + \frac{\mu_0}{\rho_0} \frac{U_0}{h^3}$$

$$\Rightarrow \boxed{U_0 = \frac{\rho_0 \alpha_0 \Delta T_0 g h^2}{\mu_0}} \Rightarrow \text{equation satisfied}$$

flow rate $Q = \int_0^h u dy = \frac{U_0}{6} \int_0^h \frac{y}{h} \left(1 - \frac{y^2}{h^2} \right) dy =$

$$= \frac{U_0 h}{6} \int_0^1 \frac{y'}{h} (1 - y'^2) dy' = \frac{U_0 h}{6} \left[\frac{y'^2}{2} - \frac{y'^4}{4} \right]_0^1 =$$

$$= \frac{U_0 h}{24}$$

VII

5

$$U \frac{\partial U}{\partial x} + V \frac{\partial U}{\partial y} = \frac{\partial}{\partial y} (-\bar{u}v) ; \frac{\partial U}{\partial x} + \frac{\partial V}{\partial y} = 0$$

$$U = U_\infty - U_1(x, y) \quad U_1 \ll U_\infty$$

$$\Rightarrow (U_\infty - U_1) \frac{\partial}{\partial x} (U_\infty - U_1) + V \frac{\partial}{\partial y} (U_\infty - U_1) = \frac{\partial}{\partial y} (-\bar{u}v)$$

$$\Rightarrow -U_\infty \frac{\partial U_1}{\partial x} - V \frac{\partial U_1}{\partial y} = \frac{\partial}{\partial y} (-\bar{u}v)$$

Since $\frac{\partial}{\partial x} (U_\infty - U_1) + \frac{\partial V}{\partial y} = 0$

$$V \sim U_1 \frac{\delta}{L} \ll U_\infty \frac{\delta}{L}$$

$$-U_\infty \frac{\partial U_1}{\partial x} - V \frac{\partial U_1}{\partial y} = \frac{\partial}{\partial y} (-\bar{u}v)$$

$$\sim \frac{U_\infty U_1}{L} \gg \frac{U_1 \delta U_1}{L \delta}$$

$$\Rightarrow \text{linearized equation } -U_\infty \frac{\partial U_1}{\partial x} = \frac{\partial}{\partial y} (-\bar{u}v)$$

with $-\bar{u}v = \beta_T U_\infty \delta w \frac{\partial}{\partial y} (U_\infty - U_1)$

$$\Rightarrow \boxed{U_\infty \frac{\partial U_1}{\partial x} = \beta_T U_\infty \delta w \frac{\partial U_1}{\partial y^2}}$$

VIII

The total force, F_x , on the body is given by

$$F_x = \rho U_\infty^2 \int_{-\infty}^{\infty} \frac{U}{U_\infty} \left(1 - \frac{U}{U_\infty} \right) dy = \rho U_\infty^2 \delta w,$$

thus δw must be constant.

thus, we have a constant turbulent

diffusivity $\nu_T = \beta_T U_\infty \delta w$ and

$$\left. \begin{aligned} U_\infty \frac{\partial U_1}{\partial x} &= \nu_T \frac{\partial^2 U_1}{\partial y^2} \\ U_1 &\rightarrow 0 \text{ as } y \rightarrow \infty \end{aligned} \right\} \text{May be solved in analogy with laminar wake.}$$

$$\frac{\partial U_1}{\partial y} = 0 \text{ at } y = 0 \quad \left\{ \text{See Recitation notes} \right.$$

$$\Rightarrow \boxed{\frac{U_1}{U_\infty} = \sqrt{\frac{\delta w}{4\pi \beta_T x}} e^{-\frac{y^2}{4\pi \beta_T x}}}$$